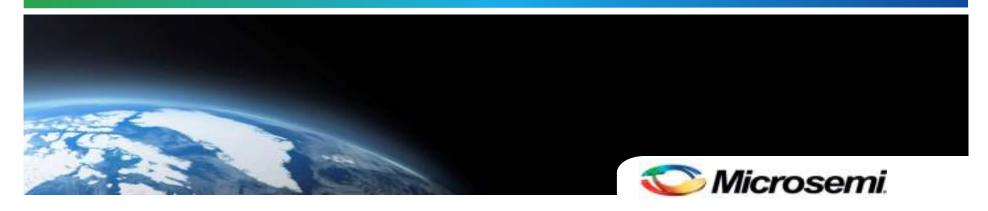
#### **Power Matters**



#### IEEE802.3 4P Task Force

## PSE PI and PD PI Pair to Pair Specifications

Rev 002

September 2014

Ottawa Canada

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## **Objectives**

- Proposing PSE PI and PD PI minimum set of unbalance parameters for having:
  - Complete specification (mathematically complete)
    - Derived from E2E\_C\_P2PRUNB
  - Implementation independent (as much as possible)
    - Ensures interoperability
  - Worst case value
    - Single value to single parameter
  - Allow flexible design of PSEs and PDs
  - Simple to use by PSE/PD designer



#### References

#### Previous work:

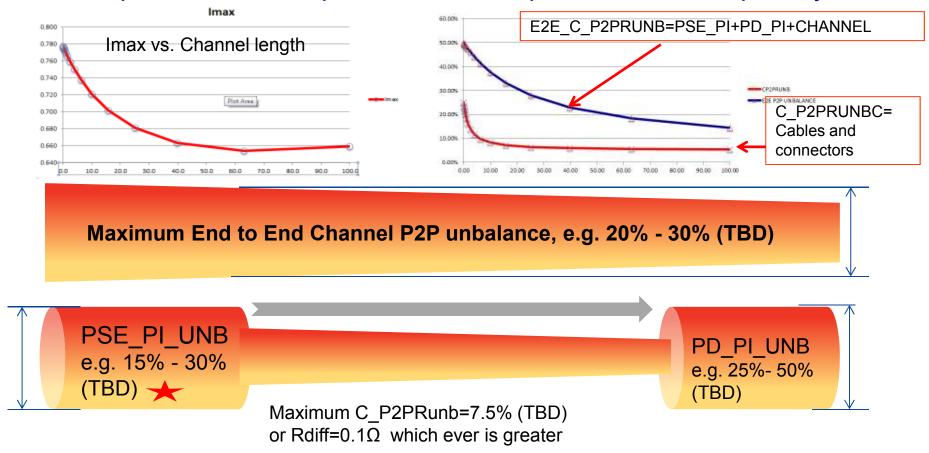
- http://www.ieee802.org/3/bt/public/jul14/Generating%20the%20PSE%20and%20PD%20PI%20models%20and%20their%20unbalance%20requirements%20rev%20013b.pdf
- Revision History:
- Rev 001:
  - Slide 9: The note at the title was updated to sync with slide 8 content.
  - Slide 17: Typo on last bullet.
- Rev 002:
- Slide 4: Adding title to the curve.
- Slide 14-17: updating numbers for sync with 0.72A max instead of 0.74A max.



## Proposal for PSE PI — Overview

-1

All parameters are specified between pairs of the same polarity



See Annex G5, G6 and G7 examples for systems with lower unbalance as well.

# Example for Existing PSE PD PI P2PRUNB Source: Annex G1, PSE PI Vdiff=0.

- Reqv=The resistance equivalent caused by P2P voltage difference on the E2E\_C\_P2PRUNB
- Rd\_eqv=The resistance equivalent caused by PD diode voltage difference and Diode dynamic resistance difference
- The following example is with PSE PI Vdiff=0.

	PSE PI PO	OS							
	Traces	Rt	Rc			Reqv	Sum	Rdiff	P2PRUNB
Rmin [ohm]	0.01	0.12	0.03			0	0.16	0.031	8.83%
Rmax [ohm]	0.011	0.13	0.05			0	0.191		
	<mark>PSE PI NE</mark>	EG							
	Traces	Rt	Rc	Rsense	RDSon	Reqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03	0.098	0.05/0.099	0	0.308/0.357	0.083/0.034	11.87%/4.55%
Rmax	0.011	0.13	0.05	0.1	0.1/0.1	0	0.391/0.391		
	PD PI POS	3							
	Traces	Rt	Rc			Rd_eqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03			0.25	0.41	0.281	25.52%
Rmax	0.011	0.13	0.05			0.5	0.691		
	PD PI NE	3							
	Traces	Rt	Rc	Rsense	RDSon	Rd_eqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03	0	0	0.25	0.41	0.281	25.52%
Rmax[ohm]	0.011	0.13	0.05	0	0	0.5	0.691		

# Example for Existing PSE PD PI P2PRUNB Source: Annex G1, PSE PI Vdiff>0.

- Reqv=The resistance equivalent caused by P2P voltage difference on the E2E\_C\_P2PRUNB
- Rd\_eqv=The resistance equivalent caused by PD diode voltage difference and Diode dynamic resistance difference
- The following example is with PSE PI Vdiff>0. P2PRUNB=(Rmax-Rmin)/(Rmax+Rmin)

	PSE PI P	OS							
	Traces	Rt	Rc			Reqv	Sum	Rdiff	P2PRUNB
Rmin [ohm]	0.01	0.12	0.03			0	0.16	0.131	29.05%
Rmax [ohm]	0.011	0.13	0.05			0.1	0.291		
	PSE PI N	EG							
	Traces	Rt	Rc	Rsense	RDSon	Reqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03	0.098	0.05	0	0.308	0.183	22.90%
Rmax	0.011	0.13	0.05	0.1	0.1	0.1	0.491		
	PD PI PO	S							
	Traces	Rt	Rc			Rd_eqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03			0.25	0.41	0.281	25.52%
Rmax	0.011	0.13	0.05			0.5	0.691		
	PD PI NE	G							
	Traces	Rt	Rc	Rsense	RDSon	Rd_eqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03	0	0	0.25	0.41	0.281	25.52%
Rmax[ohm]	0.011	0.13	0.05	0	0	0.5	0.691		

# Example for Existing PSE PD PI P2PRUNB Source: Annex G1, PSE PI Vdiff=0, PD Match diodes.

- Reqv=The resistance equivalent caused by P2P voltage difference on the E2E\_C\_P2PRUNB
- Rd\_eqv=The resistance equivalent caused by PD diode voltage difference and Diode dynamic resistance difference
- The following example is with PSE PI Vdiff=0 and PD using matched diodes. With ideal diode bridge PDE PI P2PRUNB may be a bit higher due to lower resistance and process.

	PSE PI PO	OS							
	Traces	Rt	Rc			Reqv	Sum	Rdiff	P2PRUNB
Rmin [ohm]	0.01	0.12	0.03			0	0.16	0.031	8.83%
Rmax [ohm]	0.011	0.13	0.05			0	0.191		
	PSE PI NE	EG							
	Traces	Rt	Rc	Rsense	RDSon	Reqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03	0.098	0.05/0.099	0	0.308/0.357	0.083/0.034	11.87%/4.55%
Rmax	0.011	0.13	0.05	0.1	0.1/0.1	0	0.391/0.391		
	PD PI POS	S							
	Traces	Rt	Rc			Rd_eqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03			0.225	0.385	0.056	6.78%
Rmax	0.011	0.13	0.05			0.25	0.441		
	PD PI NEC	3							
	Traces	Rt	Rc	Rsense	RDSon	Rd_eqv	Sum	Rdiff	P2PRUNB
Rmin[ohm]	0.01	0.12	0.03	0	0	0.225	0.385	0.056	6.78%
Rmax[ohm]	0.011	0.13	0.05	0	0	0.25	0.441		



## Proposal for PSE PI Solution 1 - Derivation

End to End Channel P2PRUN that sets Imax including P2P Vdiff in PSE and diode effect in PD is embedded in form of resistance in the following equation:

$$\operatorname{Im} ax = \frac{It \cdot (1 + E2E - P2PRUNB_{MAX})}{2} = \frac{It \cdot \left[1 + \frac{\left(\sum_{\substack{PSE \ R_{\text{max}}}} - \sum_{\substack{PSE \ R_{\text{min}}}}\right) + \left(\sum_{\substack{PD \ R_{\text{max}}}} - \sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{max}}}} - \sum_{\substack{R_{\text{min}}}}\right)}{2}\right]}{2}$$

■ The transformed (equivalent) PSE PI value (The real PSE PI contribution to Imax, PSE\_PI\_P2PRUNB\_eqv).

$$PSE\_PI\_P2PRUNB_{MAX}\_eqv = \frac{\left(\sum_{\substack{PSE\\R_{\text{max}}}}^{PSE} - \sum_{\substack{RSE\\R_{\text{min}}}}^{PSE}\right)}{\left(\sum_{\substack{PSE\\R_{\text{max}}}}^{PSE} + \sum_{\substack{RSE\\R_{\text{min}}}}^{PSE}\right) + \left(\sum_{\substack{R\\R_{\text{min}}}}^{PD} + \sum_{\substack{RD\\R_{\text{min}}}}^{PD}\right) + \left(\sum_{\substack{R\\R_{\text{min}}}}^{CH} + \sum_{\substack{R\\R_{\text{max}}}}^{CH}\right)}$$

The physical PSE PI P2PRUNB

$$PSE_{-}PI_{-}P2PRUNB = \frac{\left(\sum_{R_{\text{max}}}^{PSE} - \sum_{R_{\text{min}}}^{PSE}\right)}{\left(\sum_{R_{\text{max}}}^{PSE} + \sum_{R_{\text{min}}}^{PSE}\right)}$$
• We need to implement PSE PI to meet PSE\_PI\_P2PRUNB\_eqv.

$$PSE \_PI \cdot f(k, \alpha, \beta) = PSE \_PI \_P2PRUNB_{MAX} \_eqv$$

- The physical PSE PI P2PRUNB is not equal to its contribution in the system equation above as a result we need to equalize both terms above.
- For examples how to do it please see:
- http://www.ieee802.org/3/bt/public/jul14/bennett 01 0714.pdf and updated versions at E2E\_C\_P2prunb adhoc site.
- http://www.ieee802.org/3/bt/public/jul14/Generating%20the%20PSE%20and%20PD%20PI%20models%20and%20their% 20unbalance%20requirements%20rev%20013b.pdf

#### Summary -What are the minimum parameters set?

Note: All values and parameters are after transformation to fit E2CP2PRUNB behavior and limits

α, Rmax, Rmin are the effective behavior derived from system E2E\_C\_P2PRUNB

$$\alpha = \frac{\sum R \max - \sum R \min}{\sum R \max + \sum R \min} = \frac{\sum R diff}{\sum R \max + \sum R \min}$$

Option	PSE PI P2PRUNB_eqv= Rmax		Rmin Rdiff		Notes
1	α	-	-	-	Ratio.     implementation independent     Not completed
2	(Rmax-Rmin)/ (Rmax+Rmin)	Rmax	Rmin	-	Complete solution.
3	α	Rmax	Rmax*(1-α)/(1+α)		Complete solution.
4	α	$= Rmin*(1+\alpha)/(1-\alpha)$	Rmin	-	<ol> <li>Complete solution.</li> <li>Rmin is exists anyway.</li> </ol>
5	Rmin+Rdiff 0.5*Rdiff			Rdiff	Complete solution.
6	Can	't be define	Rdiff	<ol> <li>Not complete</li> <li>Implementation dependent</li> <li>Interoperability issues</li> </ol>	

- Option 1: Implementation independent but not fully mathematically complete. If Rmin is added, it is mathematically complete and will help limit pair current since Rmin exists anyway which makes it Option 4.
- Options 2-5: Complete solutions
- Option 6: Impossible

## Recommended option for PSE PI spec.

- Option 2 and option 4 are recommended as candidates. Vdiff can be addresses as separate parameter or embedded in Rmin, (Rmax).
  - Option 2: Rmax and Rmin
    - Rmax and Rmin sets PSE PI P2PRUNB.
    - No limits on Rmin. (Totally flexible design)
    - As long as Rmin is going low, Rmax will be more close to Rmin.
  - Option 4: PSE PI P2PRUNB and Rmin
    - Rmin is variable but has a minimum value. Rmin exist anyway in all PSEs and PDs (connectors, transformers traces etc.)
    - We should allow Rmin\_min as low as  $0.1\Omega$  or lower value to enable future implementations.
    - Having normative Rmin\_min in the specification help PD unbalance at short channel and allows PDs with higher unbalance currently and in the future with affecting Imax limits.
    - As long as Rmin is going low, Rmax will be more close to Rmin.

Both concepts are similar since their mathematical origin is the same and they will lead to same behavior. Option 4 allows reducing the burden on the PD by forcing minimum resistance at PSE PI and PD PI that are there anyway.



#### Proposed Specifications for PSE PI

#	Parameter	Additional Information
1	Imax continuous DC current for the pair with minimum common mode resistance	-0.72A (TBD) for Type 3 systems (In a presence of PSEP PI P2PUNB>0) -Total ALT A and ALT B current=1.2A max for type 3 systems
2	(Option 4) α=PSE_PI_P2PRUNB_EQV Value: TBD	EQV means after transformation to fit E2E_C/R_P2PRUNB limit. Value:TBD. Rmax will be calculated by Rmin_eqv*(1+α)/(1-α)
3	(Option 4 and 2) Rmin_eqv	<ul> <li>It is required for complete mathematical solution.</li> <li>(option 2) It is possible to use Rmax_eqv and Rmin_eqv per Ken's proposal which actually defines PSE_PI_P2PRUNB_EQV.</li> </ul>
4	Vdiff. Value TBD.	<ul> <li>include <u>all</u> PSE PI internal components (including of AC disconnect diode</li> <li>Implementations of diodes (AC disconnect) is controlled by Imax value that sets E2ECP2PRUNB (highest priority compared to flexible design objective)</li> <li>Vdiff may be redundant if embedded in Rmin and Rmax equivalent values by mean of 2<sup>nd</sup> transformation i.e. d_Vdiff/d_Idiff=d_Rdiff_max → P2PRUNB_equv. See: slides 40-43 at         http://www.ieee802.org/3/bt/public/unbaladhoc/Meeting 6 7 8 IEEE802 3bt Channel Pair To Pair Resistance Imbalance ad hoc rev 011a.pdf     </li> </ul>

- No need to address nonlinearities since we use single worst case unbalance parameter.
- Solution will not prevent implementing low value of sense resistor or Mosfet RDSON.



## Proposal for PD PI

- Similar way, to finalize PD PI spec.
  - PD\_PI\_P2PRUNB\_eqv parameter (after transformation to fit E2E\_C\_P2PRUNB)
  - Rmin\_eqv.
  - Or Rmax\_eqv and Rmin\_eqv

- For all options to be discussed:
  - Vdiff or Idiff as separate parameters or
  - Finding equivalent transformation from Vdiff to Rdiff by lunb\_max.
    - Values TBD.

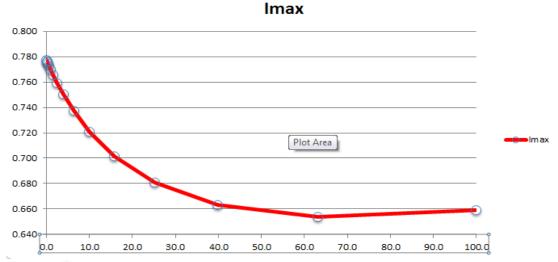
#### Details to be discussed next meeting



## New topic

#### Top down derivation of Imax and E2E C P2PRUNB

- How we define system E2E\_C\_P2PRUNB requirements
- It starts with setting maximum pair current at all operating conditions
  - Short Channel
  - Long channel
  - Minimum worst case round loop resistance of all elements
  - 12.5 $\Omega$  channel (where P2PRUNB will be minimum)
- We will look for lt/2+(1+max{Runb\_max\*lt\_min, Runb\_min\*lt\_max})/2
  - It min is the total PD current at short channel e.g. 51W/50V=1.02A
  - It\_max is the total PD current at long channel with maximum possible resistance: 1.2A





#### Top down derivation of Imax and E2E C P2PRUNB Example 1.

- Starting with high level system approach: (See simulation results in Annex G5)
- Objectives in this example: Reusing 802.3at practice (components e.g. magnetic design) resulting with the following table. (ILIM, ICUT curve allows sufficient flexibility so other numbers are possible):

Parameter [A]	Value	Additional Information
It at 1m	1.061	Sim results
It at 100m	1.170	Sim results
		Select option between 1m and
It	1.061	100m
INOM=Icut_min=	0.531	Calculation
lcut_th	0.570	(lcut_min+lcutmax)/2
Icut _max=ILIM_min	0.610	
ILIM_th	0.656	(Ilim_min+Ilim_max)/2
ILIM=	0.702	
		Actual operating point for
Imax <ilim_th< td=""><td>0.656</td><td>lmax</td></ilim_th<>	0.656	lmax
		To keep the same magjack
Actual possible Imax		etc. as in Type 2 and pre-
per current magnetics	0.720	802.3bt 4P applications
lmax=	0.720	Actual possible Imax
DI/2=	0.190	(Imax-Icut_th)/2
lmin=	0.341	lcut_th -DI/2
DI=	0.379	2xDI/2
E2E_C_P2PRUNB[%]	35.72%	DI/Icut)min =DI/It at 1m

- The PSE maximum pair current: Imax=0.72A under the following conditions
  - 4P is used
  - Total 4P current=1.2A (Type 3)

Imax=0.72A force system end to end channel effective P2P resistance unbalance=35.72% max calculated between pairs with the same polarity.

Note: Total current need to be calculated with constant power sink and round loop conditions.

> Proposed Imax=0.72A on minimum resistance pair

#### Top down derivation of Imax and E2E\_C\_P2PRUNB Example 2.

Parameter [A]	Value	Additional Information
It at 1m	1.061	Sim results
It at 100m	1.170	Sim results
It	1.170	Select option
INOM=Icut_min=	0.585	Calculation
lcut_th	0.629	(lcut_min+lcutmax)/2
lcut _max=ILIM_min	0.673	
ILIM_th	0.723	(Ilim_min+Ilim_max)/2
ILIM=	0.774	
lmax <llim_th< td=""><td>0.723</td><td>Actual operating point for Imax</td></llim_th<>	0.723	Actual operating point for Imax
Actual possible Imax		To keep the same magjack etc. as in Type 2 and pre-802.3bt 4P
per current magnetics	0.720	applications
lmax=	0.720	Actual possible Imax
DI/2=	0.135	(Imax-Icut_th)/2
Imin=	0.450	lcut_th -DI/2
DI=	0.270	2xDI/2
E2E_C_P2PRUNB[%]	23.08%	DI/Icut)min =DI/It at 1m

Worst case analysis at 100m with lowest round loop resistance

## Proposed E2E\_CHANNEL\_P2PRUNB

- Worst case analysis numbers for system End to End CP2PRUNB (to be used to allocate unbalance numbers at PSE and PD)
  - 36% (Imax=0.72A) (TBD)max at 1m
  - 15% 20% (TBD, ) max at 100m/12.5Ω
    - 24% (TBD) Max at 100m for worst case database with <12.5 Ω round loop resistance</li>



## Summary

- Two options for PSE PI speciation parameters were shown:
  - Imax definition in a presence of P2PRunb>0, 4P system
  - Specifying PSE\_PI\_RUNB\_eqv and Rmin\_eqv OR
  - Specifying Rmax\_eqv, Rmin\_eqv
  - Both options are derived via transformation from E2E\_C\_P2PRUNB
    - PSE Vdiff and diode Voltage difference and Rd difference can be specified as separate parameters or embedded in the above parameters for simpler specification.
- A methodology were shown to set the Imax and as a result the system E2E\_C\_P2PRUNB.
  - Imax is proposed to 0.72A (TBD)
  - E2ECP2PRUNB <=36% at worst case analysis and worst case end to end channel combinations.

## Reference Material

- http://www.ieee802.org/3/bt/public/unbaladhoc/Meeting 13 IEEE802 3bt Channel Pair To Pair Resist ance Imbalance ad hoc rev 017.pdf
- http://www.ieee802.org/3/bt/public/unbaladhoc/Channel%20Pair%20To%20Pair%20Resistance%20Unbalance%20Specification-What%20is%20the%20preferred%20concept.pdf
- http://www.ieee802.org/3/bt/public/unbaladhoc/Analzing\_Channel\_Pair\_To\_Pair\_Resistance\_Unbalance\_use\_cases\_rev\_6.1.pdf
- http://www.ieee802.org/3/bt/public/unbaladhoc/PI%20Balance%20Specifications%20rev%202.pdf

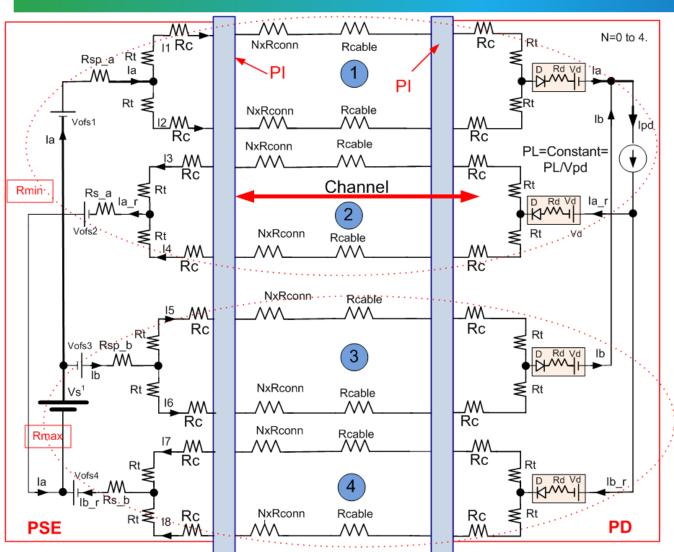


## Backup slides



#### Annex F – Model updates to be review by adhoc.

Adhoc OK: August 26, 2014



- Notes for the general Model:
- 1. Total end to end channel connectors is 6 max.
- 2. The formal channel definition is marked in red arrow and is with up to 4 connectors.
- Our work addresses also the internal application resistance of known components that are used
- 4. In simulations, pairs 1 and 2 components were set to minimum and pairs 3 and 4 were set to maximum values. See simulation results on previous meetings
- 5. Vofs1/2/3 and 4 was added. Per adhoc consensus for Vdiff. To update the group. July 3, 2014.
- 6. "Real" Diode was added to the model for investigating behavior at low currents. July 3, 2014.
- 7. The maximum number of connectors are 4. Number of connectors can varies between 0 to 4 as function of channel use cases A,B,C and D per annex G1

<sup>1.</sup> A single Vs was not meant to imply specific implementations and is drawn as single voltage source for simplification of the drawing. The important parameter is the pair to pair voltage difference.



#### Annex G1:Worst Case Data Base (updates) -1

See notes to the table in next slide

#	Parameter	Data set 1	Data set 2		
1	Cordage resistivity <sup>1</sup>	0.14Ω/m			
		0.09262Ω/m for AWG#2	4 for worst case analysis		
2	Horizontal cable resistivity option 1 <sup>2</sup>	$11.7\Omega/100$ m= $(12.5\Omega - 4*0.2\Omega)/100$ m which is the maximum resistance resulting with maximum lport.	7.92Ω/100m (CAT6A, AWG23) This is to give us maximum P2PRunb		
3	option 2 <sup>3</sup>	0.098Ω/m.			
4	Unbalance parameters	<ul> <li>Cable Pair resistance unbalance: 2%. Channel pair resistance unbalance: 3%</li> <li>Cable P2P Resistance Unbalance: 5%. Channel P2P Resistance Unbalance: 0.2Ω/6% max TBD.</li> </ul>			
5	Channel use cases to check. See figure 1 for what is a channel.	<ul> <li>A. 6 inch (0.15 m) of cordage, no connectors.</li> <li>B. 4 m channel with 1 m of cordage, 3 m of cable, 2 connectors</li> <li>C. 23 m channel with 8 m of cordage, 15 m of cable, 4 connectors</li> <li>D. 100m channel with 10 m of cordage, 90 m of cable, 4 connectors</li> </ul>			
6	End to End Channel <sup>6</sup>	The Channel per figure 1 + the PSE and	PD PIs.		
7	Transformer winding resistance	120mOhm min, 130mOhm max			
8	Connector resistance <sup>8</sup>	40mOhm min, 60mOhm max 30mOhm min, 50mOhm max			
9	Diode bridge <sup>9</sup>	Discreet Diodes: $0.39V+0.25\Omega*Id$ min; $0.53V+0.25\Omega*id$ max. (TBD)			
10	PSE output resistance <sup>10</sup>	0.25+0.1 Ohm min, 0.25+0.2 Ohm max	0.1+0.05 Ohm min, 0.1+0.1 Ohm max		

#### Annex G2: Worst case data base- Notes. -2

Per standard. It is maximum value for solid and stranded wire. The maximum value is close to AWG#26 wire resistance/meter including twist rate effects. See annex E1. Due to the fact that patch cords may use AWG#24 cables with stranded (for mechanical flexibility) or solid wire (for improved performance), we will use the AWG#24A for worst case analysis as well. Cordage with AWG#24 wire has 0.0842Ω/m for solid wire and with 10% twist rate it will be 0.09262 Ω/m.  We need both data sets (data set 1 and data set 2) to find where is the worst condition for maximum current unbalance. See Annex B curve and data showing that at short channel we get maximum P2PRUNB but it may has less concern to us since the current is lower. We need to do all use cases calculation to see where is the maximum current over the pair; at short channel or long channel. The CAT6A cable with AWG#23 has 0.066 Ω/m. Including 12% increase on cable length due to twist rate, the effective cable resistance per meter will be 1.12*6.6 Ω/100m= 0.0792 Ω/m.  Standard definition per Annex E1. We will check how results will be differ when AWG#23 is used for worst case results (lower resistance than standard definition for horizontal cable which is a maximum value.  PSE PI and PD PI includes: connector, transformer, resistors. PD PI includes diode bridge.  Connector resistance was changed since the difference (60-30) milliohm is not representing Rdiff, it is representing maximum and minimum results of connector resistance of different connectors. To correct it, we change the numbers according to inputs from connector vendors and measured data. See Annex E1-E6 for confirmation.  Yf and Rd are worst case numbers of discrete diode which there is no control on Vf and Rd. It needs more investigation to verify that we are not over specify. (Christian is checking it). Normally match components (e.g. matched two diode bridges) are used for AP operation. Any how ,PD PI spec. will eventually set the requirement.		
stranded (for mechanical flexibility) or solid wire (for improved performance), we will use the AWG#24A for worst case analysis as well. Cordage with AWG#24 wire has 0.0842Ω/m for solid wire and with 10% twist rate it will be 0.09262 Ω/m.  We need both data sets (data set 1 and data set 2) to find where is the worst condition for maximum current unbalance. See Annex B curve and data showing that at short channel we get maximum P2PRUNB but it may has less concern to us since the current is lower. We need to do all use cases calculation to see where is the maximum current over the pair; at short channel or long channel. The CAT6A cable with AWG#23 has 0.066 Ω/m. Including 12% increase on cable length due to twist rate, the effective cable resistance per meter will be 1.12*6.6 Ω/100m= 0.0792 Ω/m.  Standard definition per Annex E1. We will check how results will be differ when AWG#23 is used for worst case results (lower resistance than standard definition for horizontal cable which is a maximum value.  PSE PI and PD PI includes: connector, transformer, resistors. PD PI includes diode bridge.  Connector resistance was changed since the difference (60-30) milliohm is not representing Rdiff, it is representing maximum and minimum results of connector resistance of different connectors. To correct it, we change the numbers according to inputs from connector vendors and measured data. See Annex E1-E6 for confirmation.  Vf and Rd are worst case numbers of discrete diode which there is no control on Vf and Rd. It needs more investigation to verify that we are not over specify. (Christian is checking it). Normally match components (e.g. matched two diode bridges) are used for 4P operation. Any how ,PD PI spec. will eventually set the requirement.	1	Per standard. It is maximum value for solid and stranded wire. The maximum value is close to AWG#26 wire
<ul> <li>Annex B curve and data showing that at short channel we get maximum P2PRUNB but it may has less concern to us since the current is lower. We need to do all use cases calculation to see where is the maximum current over the pair; at short channel or long channel. The CAT6A cable with AWG#23 has 0.066 Ω/m. Including 12% increase on cable length due to twist rate, the effective cable resistance per meter will be 1.12*6.6 Ω/100m= 0.0792 Ω/m.</li> <li>Standard definition per Annex E1. We will check how results will be differ when AWG#23 is used for worst case results (lower resistance than standard definition for horizontal cable which is a maximum value.</li> <li>PSE PI and PD PI includes: connector, transformer, resistors. PD PI includes diode bridge.</li> <li>Connector resistance was changed since the difference (60-30) milliohm is not representing Rdiff, it is representing maximum and minimum results of connector resistance of different connectors. To correct it, we change the numbers according to inputs from connector vendors and measured data. See Annex E1-E6 for confirmation.</li> <li>Vf and Rd are worst case numbers of discrete diode which there is no control on Vf and Rd. It needs more investigation to verify that we are not over specify. (Christian is checking it). Normally match components (e.g. matched two diode bridges) are used for 4P operation. Any how ,PD PI spec. will eventually set the requirement.</li> </ul>		stranded (for mechanical flexibility) or solid wire (for improved performance), we will use the AWG#24A for worst case analysis as
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PSE PI and PD PI includes: connector, transformer, resistors. PD PI includes diode bridge.  Connector resistance was changed since the difference (60-30) milliohm is not representing Rdiff, it is representing maximum and minimum results of connector resistance of different connectors. To correct it, we change the numbers according to inputs from connector vendors and measured data. See Annex E1-E6 for confirmation.  Vf and Rd are worst case numbers of discrete diode which there is no control on Vf and Rd. It needs more investigation to verify that we are not over specify. (Christian is checking it). Normally match components (e.g. matched two diode bridges) are used for 4P operation. Any how ,PD PI spec. will eventually set the requirement.	3	· · · · · · · · · · · · · · · · · · ·
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that we are not over specify. (Christian is checking it). Normally match components (e.g. matched two diode bridges) are used for 4P operation. Any how ,PD PI spec. will eventually set the requirement.	8	minimum results of connector resistance of different connectors. To correct it, we change the numbers according to inputs from
10 PSE output resistance e.g. Rs_a/b=Rsense+Rdson in addition to winding resistance. See model I Annex F for reference.	9	that we are not over specify. (Christian is checking it). Normally match components (e.g. matched two diode bridges) are used for
	10	PSE output resistance e.g. Rs_a/b=Rsense+Rdson in addition to winding resistance. See model I Annex F for reference.

Adhoc response, June 24, 2014. Adhoc accept this table

Source: Yair Darshan and Christian Beia



#### Annex G5: Examples for Spice simulations for model shown in Annex F per data shown in Annex G1 with slight diode unbalance

Parameter	L=	1m	L=100m		
	I (mA)	P2PRUNB	I (mA)	P2PRUNB	
la+ (I(R41))	743.32	40.03%	649.94	11.12%	
lb+ (I(R42))	318.33	REF	519.88	REF	
Ia- (I(R20))	671.34	26.4%	633.87	8.37	
Ib- (I(R19))	390.3	REF	535.95	REF	
la total	1061.65		1169.82		
lb total	1061.65		1169.82		
Idiff_pos_max	425		130		
Idiff_neg_max	281		65		

PARAMETERS:

0.05 for Pait to Pair Run

P2PRunb = 0.05

0.02 for Pair Runb

Pair Runb = 0.02 Spice model Revision 005. Note: Ppd is constant power sink parameter model. The actual Ppd = 51

Rsense min = {Rsense max\*0.98}

PD input power (including Diode bridge is 53.339W at 100m per cable data below. ILIM = 2

Rt min = 0.12

Rdson min = 0.05

Rconn min = 0.03

Lcable = 100

Rt max = 0.13

Rsense max = 0.25

Rdson max = 0.1

Rconn max = 0.05

Resistivity = {0.1\*Cordage Resistivity+0.9\*Cable Resistivity}

Cordage\_Resistivity = 0.0926

Cable Resistivity = 0.0792

Rcable max = {Lcable\*Resistivity}

alfa = {(1-Pair Runb)/(1+Pair Runb)}

beta special = 0.925

beta =  $\{(1-P2PRunb)/(1+P2PRunb)\}$ 

-Simulation results were validated with other simulation tools and was sync with lab results. (May 2013, July 2013, August 2014).

-Components value taken from Data base Annex G1 with some changes on diode data (tighter unbalance)

Source: Yair Darshan

#### See earlier work at:

http://www.ieee802.org/3/4PPOE/public/jul13/beia 1 0713.pdf

http://www.ieee802.org/3/4PPOE/public/jul13/darshan 2 0713.pdf

http://www.ieee802.org/3/4PPOE/public/nov13/beia 01 1113.pdf

http://www.ieee802.org/3/4PPOE/public/nov13/darshan 02 1113.pdf

http://www.ieee802.org/3/4PPOE/public/nov13/darshan 03 1113.pdf

 $Vd_max = 0.1$  $Vd_min = 0$ Real diodes in simulations. Vd and Rd is used to generate unbalance.

Rd max = 0.1Rd min = 0.0001



#### Annex G6: Examples for Spice simulations for model shown in Annex F per data shown in Annex G1 with PD identical diodes/ Ideal Diode Bridge(\*)

Parameter	L=	1m	L=100m		
	I (mA)	P2PRUNB	I (mA)	P2PRUNB	
la+ (I(R41))	562.2 / 564.6	5.9% / 10.6%	630 / 602	7.73% / 8.12%	
lb+ (I(R42))	499.6 / 456.2	REF	540 / 512	REF	
la- (I(R20))	567.2 / 557.7	6.8%/9.3%	617 / 588	5.4% / 5.6%	
lb- (I(R19))	494.7 / 463	REF	554 / 526	REF	
la total	1061.82 / 1020.8		1170 /1114		
lb total	1061.82 / 1020.8		1170/1114		
Idiff_pos_max	62.6		90.4 / 90		
Idiff_neg_max	72.45		62.3 / 62		

PARAMETERS:

P2PRunb = 0.050.02 for Pair Runb

Pair Runb = 0.02

Spice model Revision 005. Note: Ppd is constant power sink parameter model. The actual Ppd = 51

PD input power (including Diode bridge is 51W+diode power loss. ILIM = 2

Lcable = 100

Resistivity = {0.1\*Cordage Resistivity+0.9\*Cable Resistivity}

Cordage\_Resistivity = 0.0926

Cable Resistivity = 0.0792

Rcable max = {Lcable\*Resistivity}

0.05 for Pait to Pair Run

alfa = {(1-Pair Runb)/(1+Pair Runb)} beta = {(1-P2PRunb)/(1+P2PRunb)}

beta special = 0.925

Simulation results were validated with other simulation tools and were sync with lab results. (August 2014). Components value taken from Data base Annex G1 with some changes on diode data (tighter unbalance)

Source: Yair Darshan

Rt max = 0.13Rt min = 0.12

Rsense max = 0.25 Rsense min = {Rsense max\*0.98}

Rdson max = 0.1Rdson min = 0.05

Rconn max = 0.05Rconn min = 0.03

Vd max = 0.01Vd min = 0.01 See earlier work at:

http://www.ieee802.org/3/4PPOE/public/jul13/beia 1 0713.pdf

http://www.ieee802.org/3/4PPOE/public/jul13/darshan 2 0713.pdf

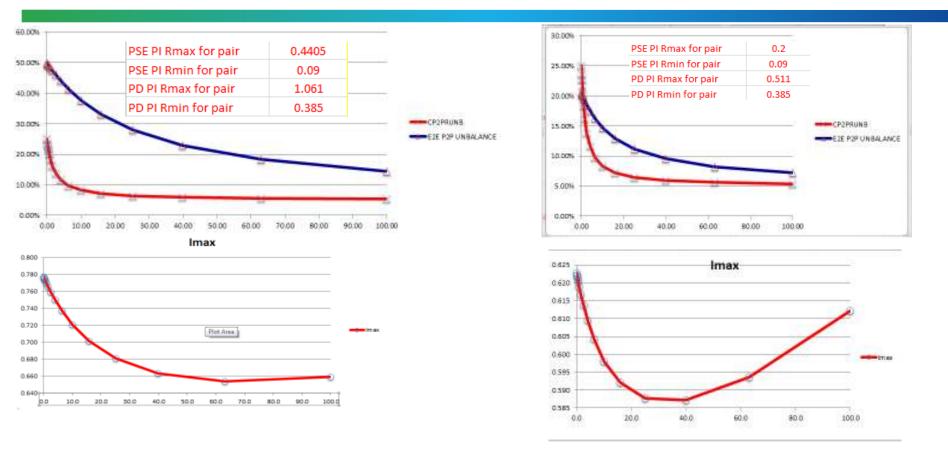
http://www.ieee802.org/3/4PPOE/public/nov13/beia 01 1113.pdf

http://www.ieee802.org/3/4PPOE/public/nov13/darshan 02 1113.pdf http://www.ieee802.org/3/4PPOE/public/nov13/darshan 03 1113.pdf

Rd max = 0.1(\*) For ideal diode bridge: Diode model was shorted by 0.01 ohm. Vd max/min=0.01V, Rd max/min=0.1 Rd min = 0.1



Annex G7: Comparison System End to End Channel P2PRUNB and Channel only P2PRUNB per Annex F model with two examples of PSE and PD Rmax, Rmin values that represents PSE and PD PI P2PRUNB. Data taken from Annex G1.



- Left side plots:
- PSE and PD with high unbalance
- System P2PRUNB way above Channel P2PRUNB
- System: ~50% at short channel, 15% at 100m
- Channel: 25% max short channel (Rdiff<0.1Ω), %5.5% at 100m

- Right side plots:
- PSE and PD with moderate unbalance
- System P2PRUNB regulates channel at short channels.
- System: ~20% at short channel 7.5% at 100m
- Channel: 25% max short channel (Rdiff<0.1Ω), %5.5% at 100m</li>

Source: Yair Darshan. Tools: Excel. Confirmation tool: MATLAB



## Annex L1: What are the options for complete specification for unbalance PSE PI and PD PI models parameters



#### Source: Yair Darshan. June 25, 2014

- Current unbalance is a function of Voltage unbalance and resistance unbalance between pairs.
  - These are the only parameters that affect the current unbalance and as a result the maximum pair current due to the unbalance situation.
- For simplicity let's assume Voltage unbalance is zero. We will address the effect of Voltage difference later.
- By definition, the current unbalance between any two pairs is:

$$\begin{split} Idiff &= \left| I_{1} - I_{2} \right| = It \cdot \frac{\sum R_{\text{max}}}{\sum R_{\text{max}} + \sum R_{\text{min}}} - It \cdot \frac{\sum R_{\text{min}}}{\sum R_{\text{max}} + \sum R_{\text{min}}} = It \cdot \left( \frac{\sum R_{\text{max}} - \sum R_{\text{min}}}{\sum R_{\text{max}} + \sum R_{\text{min}}} \right) \\ &\frac{Idiff}{It} = \left( \frac{\sum R_{\text{max}} - \sum R_{\text{min}}}{\sum R_{\text{max}} + \sum R_{\text{min}}} \right) = Runb = Iunb \end{split}$$

- Since we are discussing P2P unbalance the Runb and lunb is between Pair to Pair and the sum of R1 and the sum of R2 represents two wires in parallel including all components connected to each wire.
- The above equations are the same for PSE PI, Channel and PD PI unbalance. The difference is the content of R1 and R2 e.g. for channel it is just cables and connectors. For PSE and PD PIs it contains additional other components such MOSFETs, Diodes, Transformers etc.

#### Annex L2: What are the options for complete specification for unbalance PSE PI and PD PI models parameters

- The maximum pair current is function of the total End to End Channel Resistance and Voltage Unbalance.
- The PSE PI and PD PI are affecting Imax at short and long channels.
- By definition for maximum pair current Imax as function of P2PRUNB and P2P Voltage Difference of the system from end to end:

$$\operatorname{Im} ax = \frac{\operatorname{It}}{2} + \frac{\operatorname{It} \cdot E2E - P2PRUNB}{2} = \frac{\operatorname{It} \cdot (1 + E2E - P2PRUNB)}{2}$$

$$\operatorname{Im} ax = \frac{It \cdot (1 + E2E - P2PRUNB)}{2} = \frac{It \cdot \left[1 + \frac{\left(\sum_{\substack{PSE \ R_{\text{max}}}} - \sum_{\substack{PSE \ R_{\text{min}}}}\right) + \left(\sum_{\substack{PD \ R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack{R_{\text{min}}}}\right) + \left(\sum_{\substack$$

$$\operatorname{Im} ax = \frac{\operatorname{It} \cdot (1 + E2E - P2PRUNB)}{2} = \frac{\operatorname{It} \cdot \left[ 1 + \left( \frac{\sum_{\substack{PSE \\ R_{\text{max}}}} \sum_{\substack{PSE \\ R_{\text{max}}}} + \sum_{\substack{PD \\ R_{\text{max}}}} + \sum_{\substack{PSE \\ R_{\text{max}}}} + \sum_{\substack{PSE \\ R_{\text{min}}}} + \sum_{\substack{PD \\ R_{\text{min}}}}$$

- The PSE PI P2PRUNB can be defined in similar way by similarity.
- Note: PSE PI P2PRUNB is not equal to E2E CPWPRUNB nor to PD PI P2PRUN. It requires additional mathematical procedure to find this parameters so it will be equal to the E2E CP2PRUNB target. Source: Yair Darshan

## Annex L3: What are the options for complete specification for unbalance PSE PI and PD PI models parameters

We can see that Imax is function of Rmax and Rmin and Rdiff=Rmax-Rmin

$$\operatorname{Im} ax = \frac{\operatorname{It} \cdot (1 + E2E - P2PRUNB)}{2} = \frac{\operatorname{It} \cdot \left[ 1 + \left( \frac{\sum_{\substack{PSE \ R_{\text{max}}}} \sum_{\substack{PSE \ R_{\text{max}}}} + \sum_{\substack{PD \ R_{\text{max}}}} + \sum_{\substack{PSE \ R_{\text{min}}}} + \sum_{\substack{PD \ R_{\text{min}}} + \sum_{\substack{PD \ R_{\text{min}}}} + \sum_{\substack{PD \ R_{\text{min}}}} + \sum_{\substack{PD \ R_{\text{min}}}} + \sum_{\substack{PD \ R_{\text{min}}} + \sum_{\substack$$

 From the above, PSE PI P2PRUNB upper limit can be extracted and it will have the same effect on Imax with the same exact concept.

$$PSE - PI - P2PRUNB = \frac{\sum_{R_{diff}}^{PSE}}{\sum_{R_{max}}^{PSE} + \sum_{R_{max}}^{PD} + \sum_{R_{min}}^{CH} + \sum_{R_{min}}^{PSE} + \sum_{R_{min}}^{PD} + \sum_{R_{min}}^{CH}}$$

$$PSE\_PI\_P2PRUNB = \frac{(k+\alpha) \cdot \sum_{\substack{R_{diff}}}^{PSE}}{\sum_{\substack{R_{max}}}^{PSE} + \sum_{\substack{R_{min}}}^{PSE} + \beta} = \frac{\sum_{\substack{R_{diff}}}^{PSE}}{\sum_{\substack{R_{max} \\ R_{min}}}^{PSE} + \sum_{\substack{R_{min} \\ R_{min}}}^{PSE}}$$

- The terms k, a and b are used to transform the true PSE PI P2PRUNB to PSE PI P2PRUNB as stand alone function.
- Now we can see what are the necessary unbalanced properties that are needed to uniquely specify the PSE PI?
  Source: Yair Darshan

## Annex L4: What are the options for complete specification for unbalance PSE PI and PD PI models parameters

$$PSE\_PI\_P2PRUNB = \frac{\sum_{\substack{R_{diff}\_new}}^{PSE}}{\sum_{\substack{R_{max}\_new}}^{PSE}} + \sum_{\substack{R_{min}\_new}}^{PSE}} = \frac{\sum_{\substack{R_{max}\_new}}^{PSE}}{\sum_{\substack{R_{max}\_new}}^{PSE}} + \sum_{\substack{R_{min}\_new}}^{PSE}}$$

$$Im \ ax = 0.5 \cdot It \cdot \left(1 + \frac{\sum_{\substack{R_{diff}\_new}}^{PSE}}{\sum_{\substack{R_{min}\_new}}^{PSE}} + \sum_{\substack{R_{min}\_new}}^{PSE}}\right)$$

- Conclusions: In order to limit Imax\_pair you must have in addition to voltage difference and maximum load current It, two additional parameters.
- Firs and fast observation: Imax is equation with 3 parameters. Total current, It is given. We need two variable to solve equation with two parameters
- So specifying only Rdiff and Vdiff for PSE PI or PD PI will not work. It leads to interoperability issues. (one parameter is loose..)



## Annex L5: What are the options for complete specification for unbalance PSE PI and PD PI models parameters

- Imax is direct function of PSE PI RUNB and Channel and PD parts.
- The transformed PSE\_PI\_P2PRUNB\_new control Imax.

$$\operatorname{Im} ax = 0.5 \cdot \operatorname{It} \cdot \left(1 + \operatorname{PSE} \operatorname{PI} \operatorname{P2PRUNB} \operatorname{new}\right) = 0.5 \cdot \operatorname{It} \cdot \left(1 + \frac{\sum_{\substack{R \text{odiff} \ new}}^{PSE}}{\sum_{\substack{R \text{max} \ new}}^{PSE}} + \sum_{\substack{R \text{min} \ new}}^{PSE}}\right)$$

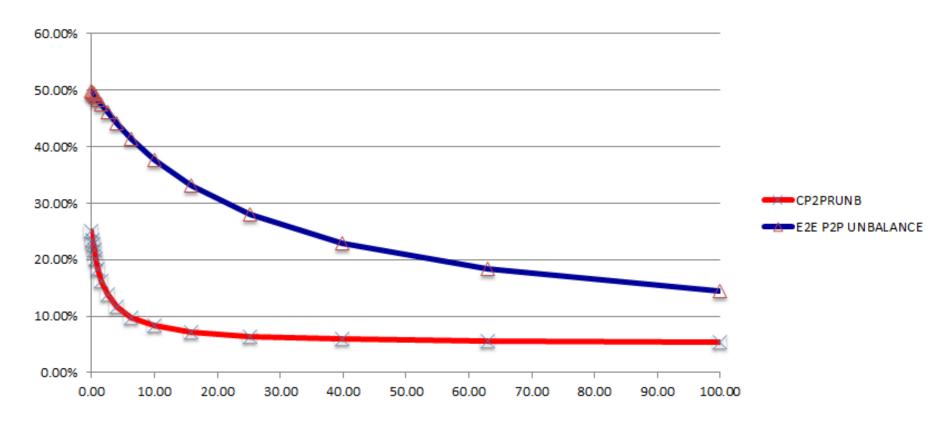
- If we specify PSE PI by only Rdiff and Vdiff we will have the following interoperability issues:
- Examples:
- Rdiff=Rmax-Rmin=0.2=X:
  - P2PRUNB=(0.2-0)/(0.2+0)=100%
  - P2PRUNB=(0.23-0.03)/(0.23+0.03)=77%
  - P2PRUNB=(0.3-0.1)/(0.3+0.1)=50%
  - P2PRUNB=(1-0.8)/(1+0.8)=11%

Interoperability Issue:
Different UNBALANCE
For the same Rdiff resulting
With different Imax for the
Same channel and PD

Source: Yair Darshan

# Annex R: End to End Channel P2PRUNB vs Channel P2PRUNB

- Using adhoc database values for components. Annex G1.
- The high C\_P2PRUNB at short cable at short cable is dominate by PSE PI and PD PI components.





## Annex R1: Maximum pair current

- Using adhoc database values for components. Annex G1.
- The high C\_P2PRUNB at short cable at short cable is dominate by PSE PI and PD PI components.

#### **Imax**

